

**Unconsolidated Undrained (UU)**Project Name: **BYU (Dr. Youd)**

Project Number:

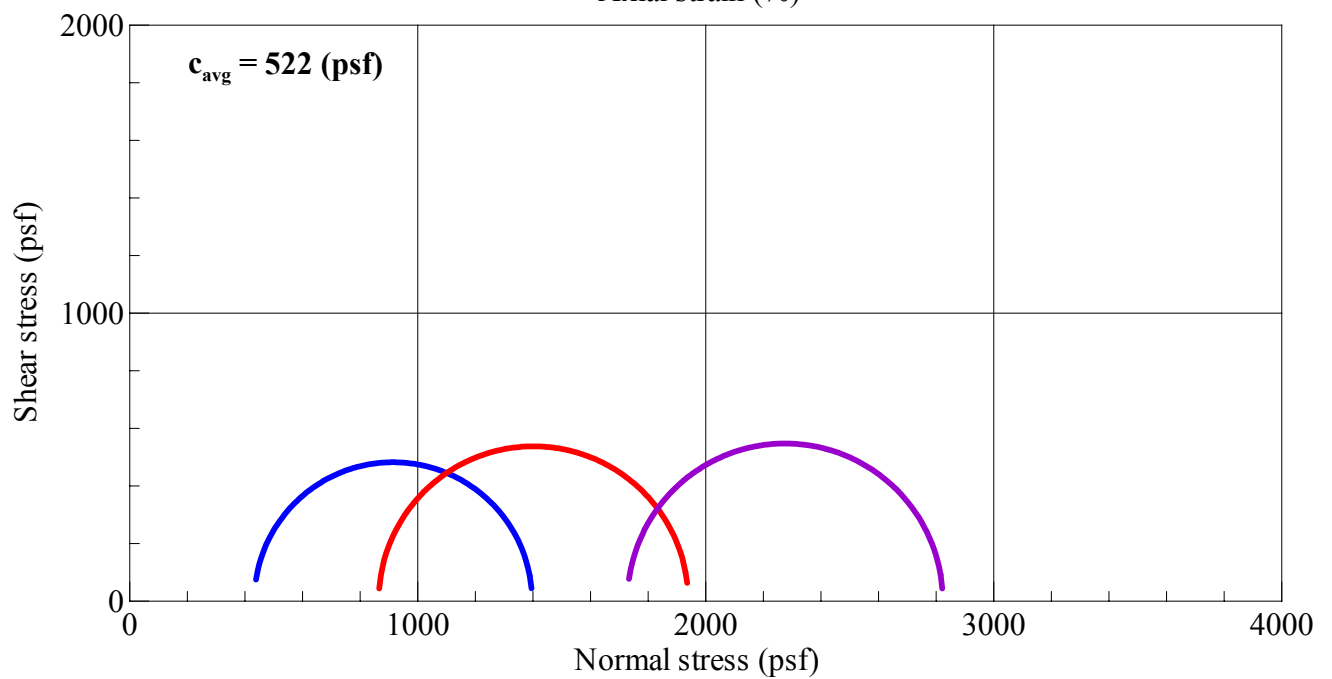
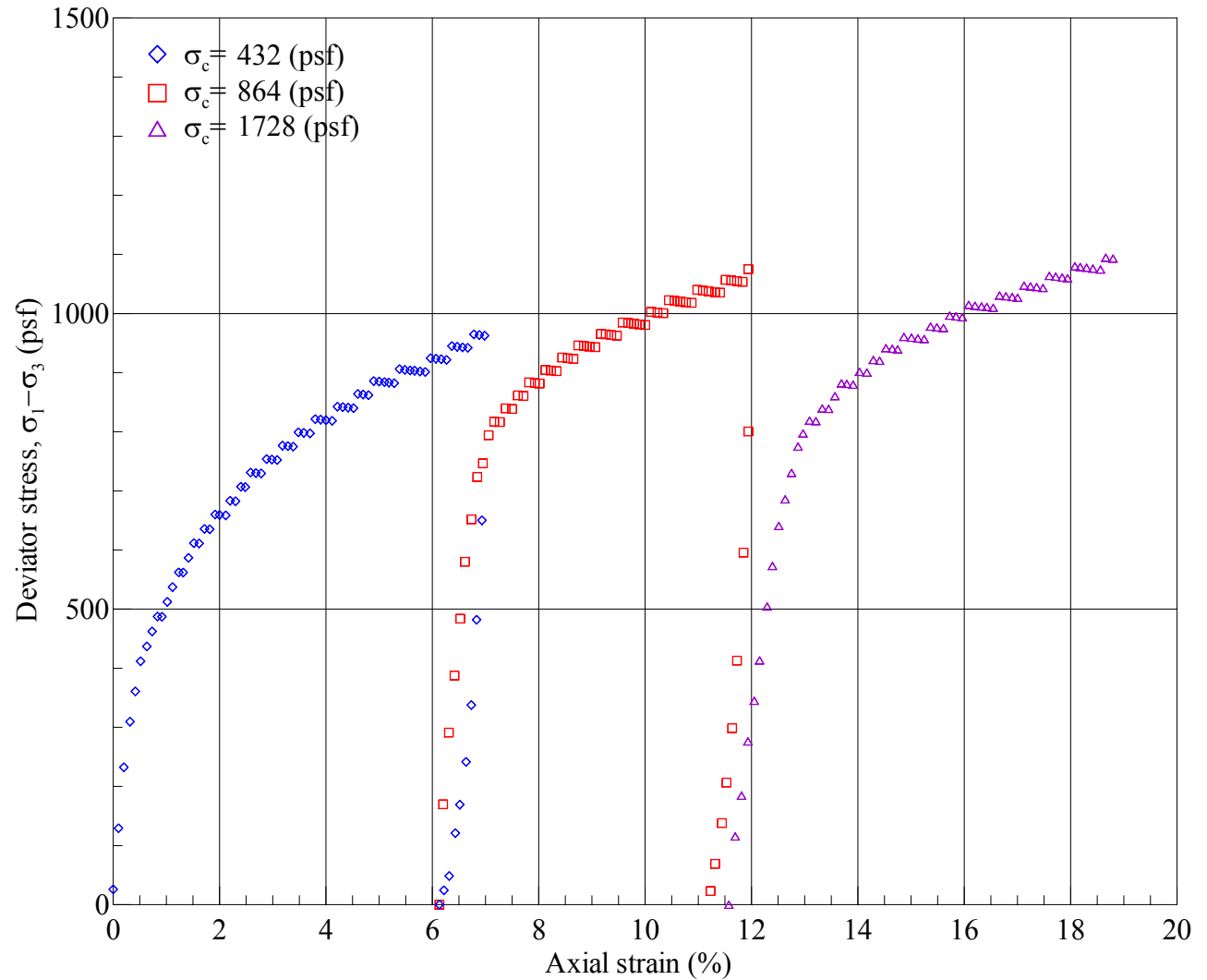
Sample: **WLA D2**Depth: **5-7.5**

Phase			1		2		3			
Initial		w (%)	32.1		Multi-Staged Test					
		$\gamma_m$ (pcf)	123.9							
		$\gamma_d$ (pcf)	93.8							
		B	0.9							
Final		w (%)							33.6	
		$\gamma_m$ (pcf)							130.6	
		$\gamma_d$ (pcf)							97.8	
		B							0.97	
Back pressure (psi)			24.5		24.5		24.5			
Strain rate (in/min)			0.0180		0.0180		0.0180			
Stress conditions			Peak $\sigma_1 - \sigma_3$	Max $\sigma'_1 / \sigma'_3$	Peak $\sigma_1 - \sigma_3$	Max $\sigma'_1 / \sigma'_3$	Peak $\sigma_1 - \sigma_3$	Max $\sigma'_1 / \sigma'_3$		
Total Stress at Failure	Time to Fail (min)		23.0		18.7		20.3			
	$\epsilon$ (%)		6.78		11.94		18.66			
	$\sigma_3$ (psf)		432		864		1728			
	$\sigma_1 - \sigma_3$ (psf)		965		1075		1095			
	$\sigma_1$ (psf)		1397		1939		2823			
	$P = (\sigma_1 + \sigma_3) / 2$ (psf)		914		1402		2275			
	$Q = (\sigma_1 - \sigma_3) / 2$ (psf)		482		538		547			
	Shear stress at failure, $\tau_f$ (psf)		482		538		547			

Average shear stress at failure, $\tau_f$ (psf)	522
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Tested by: \_\_\_\_\_

Reviewed: \_\_\_\_\_



**Multi-Staged Triaxial Test**  
**Unconsolidated Undrained (UU)**



Project: **BYU (Dr. Youd)**

Phase 1

Number: **M00399-003**

Confining Stress = 432 (psf)

Sample: **WLA D2**

Depth: **5-7.5**

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Axial strain, $\epsilon$ (%)	$\sigma_d$ ( $\sigma_1 - \sigma_3$ ) (psf)	Total $\sigma_3$ (psf)	Total $\sigma_1$ (psf)	$Q = s_u$ ( $\sigma_1 - \sigma_3$ )/2 (psf)	$P$ ( $\sigma_1 + \sigma_3$ )/2 (psf)	$\sigma_1/\sigma_3$
0.00	26	432	458	13	445	1.06
0.10	129	432	561	65	497	1.30
0.20	232	432	664	116	548	1.54
0.32	310	432	742	155	587	1.72
0.42	361	432	793	180	612	1.84
0.52	412	432	844	206	638	1.95
0.63	437	432	869	219	651	2.01
0.73	462	432	894	231	663	2.07
0.83	488	432	920	244	676	2.13
0.92	487	432	919	244	676	2.13
1.02	512	432	944	256	688	2.19
1.12	537	432	969	269	701	2.24
1.23	562	432	994	281	713	2.30
1.32	562	432	994	281	713	2.30
1.42	587	432	1019	293	725	2.36
1.52	612	432	1044	306	738	2.42
1.62	611	432	1043	305	737	2.41
1.72	636	432	1068	318	750	2.47
1.82	635	432	1067	318	750	2.47
1.92	660	432	1092	330	762	2.53
2.00	659	432	1091	330	762	2.53
2.12	659	432	1091	329	761	2.52
2.20	683	432	1115	342	774	2.58
2.30	683	432	1115	341	773	2.58
2.40	707	432	1139	354	786	2.64
2.48	707	432	1139	353	785	2.64
2.58	731	432	1163	366	798	2.69
2.68	730	432	1162	365	797	2.69
2.78	730	432	1162	365	797	2.69
2.88	754	432	1186	377	809	2.75
2.98	753	432	1185	377	809	2.74
3.08	752	432	1184	376	808	2.74
3.18	777	432	1209	388	820	2.80
3.28	776	432	1208	388	820	2.80
3.38	775	432	1207	388	820	2.79
3.48	799	432	1231	400	832	2.85
3.58	798	432	1230	399	831	2.85
3.70	797	432	1229	399	831	2.85
3.80	821	432	1253	411	843	2.90
3.90	821	432	1253	410	842	2.90
4.00	820	432	1252	410	842	2.90
4.12	819	432	1251	409	841	2.90
4.22	843	432	1275	421	853	2.95
4.32	842	432	1274	421	853	2.95
4.42	841	432	1273	420	852	2.95
4.52	840	432	1272	420	852	2.94
4.60	864	432	1296	432	864	3.00
4.70	863	432	1295	432	864	3.00
4.80	862	432	1294	431	863	3.00
4.90	886	432	1318	443	875	3.05
5.00	885	432	1317	442	874	3.05
5.10	884	432	1316	442	874	3.05
5.18	883	432	1315	442	874	3.04
5.28	882	432	1314	441	873	3.04
5.38	906	432	1338	453	885	3.10
5.48	905	432	1337	452	884	3.09
5.58	904	432	1336	452	884	3.09
5.67	903	432	1335	452	884	3.09
5.77	902	432	1334	451	883	3.09
5.87	901	432	1333	451	883	3.09
5.97	925	432	1357	462	894	3.14
6.07	924	432	1356	462	894	3.14
6.17	923	432	1355	461	893	3.14
6.27	922	432	1354	461	893	3.13
6.37	945	432	1377	472	904	3.19
6.47	944	432	1376	472	904	3.18
6.57	943	432	1375	471	903	3.18

Project: **BYU (Dr. Youd)**

Phase 1

Number: **M00399-003**

Confining Stress = 432 (psf)

Sample: **WLA D2**

Depth: **5-7.5**

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Axial strain, $\epsilon$ (%)	$\sigma_d$ ( $\sigma_1 - \sigma_3$ ) (psf)	Total $\sigma_3$ (psf)	Total $\sigma_1$ (psf)	$Q = s_u$ ( $\sigma_1 - \sigma_3$ )/2 (psf)	$P$ ( $\sigma_1 + \sigma_3$ )/2 (psf)	$\sigma_1/\sigma_3$
6.67	942	432	1374	471	903	3.18
6.78	965	432	1397	482	914	3.23
6.88	964	432	1396	482	914	3.23
6.98	963	432	1395	481	913	3.23
6.93	650	432	1082	325	757	2.51
6.83	482	432	914	241	673	2.12
6.73	338	432	770	169	601	1.78
6.63	242	432	674	121	553	1.56
6.52	169	432	601	85	517	1.39
6.43	121	432	553	61	493	1.28
6.32	48	432	480	24	456	1.11
6.22	24	432	456	12	444	1.06
6.13	0	432	432	0	432	1.00

**Multi-Staged Triaxial Test**  
**Unconsolidated Undrained (UU)**



Project: **BYU (Dr. Youd)**  
 Number: **M00399-003**  
 Sample: **WLA D2**  
 Depth: **5-7.5**

Phase 2  
 Confining Stress = 864 (psf)

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Axial strain, $\epsilon$ (%)	$\sigma_d$ ( $\sigma_1 - \sigma_3$ ) (psf)	Total $\sigma_3$ (psf)	Total $\sigma_1$ (psf)	Q = $s_u$ ( $\sigma_1 - \sigma_3$ )/2 (psf)	P ( $\sigma_1 + \sigma_3$ )/2 (psf)	$\sigma_1/\sigma_3$
6.13	0	864	864	0	864	1.00
6.20	170	864	1034	85	949	1.20
6.31	291	864	1155	145	1009	1.34
6.42	388	864	1252	194	1058	1.45
6.52	484	864	1348	242	1106	1.56
6.61	580	864	1444	290	1154	1.67
6.74	652	864	1516	326	1190	1.75
6.84	724	864	1588	362	1226	1.84
6.95	747	864	1611	373	1237	1.86
7.06	794	864	1658	397	1261	1.92
7.16	817	864	1681	409	1273	1.95
7.27	816	864	1680	408	1272	1.94
7.38	840	864	1704	420	1284	1.97
7.50	838	864	1702	419	1283	1.97
7.61	862	864	1726	431	1295	2.00
7.71	861	864	1725	430	1294	2.00
7.82	884	864	1748	442	1306	2.02
7.93	883	864	1747	441	1305	2.02
8.02	882	864	1746	441	1305	2.02
8.12	905	864	1769	452	1316	2.05
8.23	904	864	1768	452	1316	2.05
8.34	903	864	1767	451	1315	2.04
8.44	925	864	1789	463	1327	2.07
8.55	924	864	1788	462	1326	2.07
8.65	923	864	1787	462	1326	2.07
8.74	946	864	1810	473	1337	2.10
8.85	945	864	1809	473	1337	2.09
8.96	944	864	1808	472	1336	2.09
9.06	943	864	1807	472	1336	2.09
9.17	966	864	1830	483	1347	2.12
9.26	965	864	1829	482	1346	2.12
9.36	964	864	1828	482	1346	2.12
9.47	963	864	1827	481	1345	2.11
9.58	985	864	1849	493	1357	2.14
9.68	984	864	1848	492	1356	2.14
9.79	983	864	1847	491	1355	2.14
9.90	982	864	1846	491	1355	2.14
10.00	981	864	1845	490	1354	2.14
10.11	1003	864	1867	501	1365	2.16
10.23	1002	864	1866	501	1365	2.16
10.34	1000	864	1864	500	1364	2.16
10.45	1023	864	1887	511	1375	2.18
10.55	1021	864	1885	511	1375	2.18
10.66	1020	864	1884	510	1374	2.18
10.77	1019	864	1883	510	1374	2.18
10.87	1018	864	1882	509	1373	2.18
10.98	1040	864	1904	520	1384	2.20
11.09	1039	864	1903	519	1383	2.20
11.19	1038	864	1902	519	1383	2.20
11.32	1036	864	1900	518	1382	2.20
11.41	1035	864	1899	518	1382	2.20
11.51	1057	864	1921	529	1393	2.22
11.62	1056	864	1920	528	1392	2.22
11.73	1055	864	1919	527	1391	2.22
11.83	1054	864	1918	527	1391	2.22
11.94	1075	864	1939	538	1402	2.24
11.94	801	864	1665	400	1264	1.93
11.85	595	864	1459	298	1162	1.69
11.73	413	864	1277	206	1070	1.48
11.64	298	864	1162	149	1013	1.35
11.53	207	864	1071	103	967	1.24
11.44	138	864	1002	69	933	1.16
11.32	69	864	933	35	899	1.08
11.23	23	864	887	12	876	1.03
11.12	-23	864	841	-12	852	0.97
11.02	-46	864	818	-23	841	0.95

**Multi-Staged Triaxial Test**  
**Unconsolidated Undrained (UU)**



Project: **BYU (Dr. Youd)**  
 Number: **M00399-003**  
 Sample: **WLA D2**  
 Depth: **5-7.5**

Phase 3  
 Confining Stress = 1728 (psf)

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Axial strain, $\epsilon$ (%)	$\sigma_d$ ( $\sigma_1 - \sigma_3$ ) (psf)	Total $\sigma_3$ (psf)	Total $\sigma_1$ (psf)	Q = $s_u$ ( $\sigma_1 - \sigma_3$ )/2 (psf)	P ( $\sigma_1 + \sigma_3$ )/2 (psf)	$\sigma_1/\sigma_3$
11.57	0	1728	1728	0	1728	1.00
11.69	115	1728	1843	58	1786	1.07
11.81	184	1728	1912	92	1820	1.11
11.93	276	1728	2004	138	1866	1.16
12.05	345	1728	2073	172	1900	1.20
12.15	413	1728	2141	207	1935	1.24
12.29	505	1728	2233	252	1980	1.29
12.39	573	1728	2301	286	2014	1.33
12.51	641	1728	2369	320	2048	1.37
12.63	686	1728	2414	343	2071	1.40
12.75	731	1728	2459	365	2093	1.42
12.87	775	1728	2503	388	2116	1.45
12.97	797	1728	2525	399	2127	1.46
13.09	819	1728	2547	410	2138	1.47
13.21	818	1728	2546	409	2137	1.47
13.33	840	1728	2568	420	2148	1.49
13.45	839	1728	2567	419	2147	1.49
13.57	860	1728	2588	430	2158	1.50
13.69	882	1728	2610	441	2169	1.51
13.79	881	1728	2609	441	2169	1.51
13.91	880	1728	2608	440	2168	1.51
14.03	901	1728	2629	451	2179	1.52
14.17	900	1728	2628	450	2178	1.52
14.29	922	1728	2650	461	2189	1.53
14.41	920	1728	2648	460	2188	1.53
14.53	942	1728	2670	471	2199	1.54
14.65	941	1728	2669	470	2198	1.54
14.75	940	1728	2668	470	2198	1.54
14.87	961	1728	2689	480	2208	1.56
15.01	959	1728	2687	480	2208	1.56
15.13	958	1728	2686	479	2207	1.55
15.25	957	1728	2685	478	2206	1.55
15.37	978	1728	2706	489	2217	1.57
15.49	977	1728	2705	488	2216	1.57
15.61	976	1728	2704	488	2216	1.56
15.73	996	1728	2724	498	2226	1.58
15.84	995	1728	2723	498	2226	1.58
15.96	994	1728	2722	497	2225	1.58
16.08	1015	1728	2743	507	2235	1.59
16.20	1014	1728	2742	507	2235	1.59
16.32	1012	1728	2740	506	2234	1.59
16.42	1011	1728	2739	506	2234	1.59
16.54	1010	1728	2738	505	2233	1.58
16.66	1031	1728	2759	515	2243	1.60
16.78	1029	1728	2757	515	2243	1.60
16.90	1028	1728	2756	514	2242	1.59
17.00	1027	1728	2755	513	2241	1.59
17.12	1047	1728	2775	524	2252	1.61
17.24	1046	1728	2774	523	2251	1.61
17.36	1045	1728	2773	522	2250	1.60
17.48	1043	1728	2771	522	2250	1.60
17.60	1064	1728	2792	532	2260	1.62
17.72	1062	1728	2790	531	2259	1.61
17.84	1061	1728	2789	531	2259	1.61
17.94	1060	1728	2788	530	2258	1.61
18.08	1080	1728	2808	540	2268	1.63
18.18	1079	1728	2807	539	2267	1.62
18.30	1077	1728	2805	539	2267	1.62
18.42	1076	1728	2804	538	2266	1.62
18.56	1074	1728	2802	537	2265	1.62
18.66	1095	1728	2823	547	2275	1.63
18.80	1093	1728	2821	547	2275	1.63